



Streamlining Warm Way Of Behaving Of Conservative Intensity Exchanger

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Abstract

One of the most important aspects of machines, devices, and industrial processes that keeps their functionality and improves product quality is heat transfer. In order to maintain the desired operating temperatures and dissipate additional heat from the process or device, heat exchangers of various types and sizes are utilized in these applications. However, because it determines the space (i.e. the size) of the machine, device, or treatment plant, the size of a heat exchanger is an essential consideration for any kind of process or device. The motivation behind this study is, most importantly, to hypothetically look at the plan cycle of an intensity exchanger, then to break down and upgrade its presentation utilizing PC helped liquid elements. A counter-current intensity exchanger was considered for configuration purposes and its length was hypothetically determined utilizing the LMTD strategy, while the strain drop and energy utilization were likewise determined with the Kern technique. The behavior of heat transfer, mass flow rates, pressure drops, flow velocities, and vortices of the bundle flows in the heat exchanger was analyzed using the three-case model in the CFD analysis in this study. Hypothetical and CFD results showed just a 1.15% distinction in the cooling execution of hot liquids. The hub pressure drops showed positive connections with the absolute intensity move coefficient and the required siphoning power. Generally speaking, the consequences of this review affirm that CFD displaying can be promising for the plan and advancement of intensity exchangers and that it can test many plan choices without creating actual models.

Keywords: CFD, Heat Exchanger, LMTD, ANSYS.

INTRODUCTION

Heat exchangers are among the most regularly involved gadgets in the process business. Heat is transferred between two process flows through heat exchangers. Their utilization shows that any interaction including cooling, warming, buildup, bubbling, or vanishing requires an intensity exchanger for this reason. Prior to undergoing a phase change in the processor, process liquids are typically heated or cooled. Different intensity exchangers are named by their application. For instance, the intensity exchangers utilized for buildup are called condensers, similarly the intensity exchangers for cooking are called boilers. The presentation and productivity of intensity exchangers are estimated utilizing how much intensity move utilizing the more modest intensity move region and the tension drop [1]-[2]. Effectiveness can best be addressed by working out the complete intensity move coefficient. An overview of a heat exchanger's

investment costs and energy requirements (operating costs) is provided by the pressure drop and the required area for a particular heat transfer.

A. *Heat exchangers are of two types*

- If the two fluids between which heat is exchanged are in direct contact with each other, the heat exchanger is in direct contact.
- If the two fluids are separated by a wall through which heat is transferred so that they never mix, contact the heat exchangers with indirect contact.

A typical heat exchanger, typically for applications with higher pressures up to 552 bar, is the tube bundle heat exchanger. Tube bundle heat exchanger, indirect contact heat exchanger. It consists of a series of tubes through which one of the liquids flows. The bowl is the container for the bowl liquid. In general, it has a cylindrical shape with a circular section, although in some applications shells of different shapes are used. For this particular study, a hull is considered, which a single-passage hull [3] is generally. A shell is often used because of its low cost and simplicity and has the highest correction factor for the log- mean temperature difference (LMTD). Although the tubes may have one or more passages, there is a passage on the side of the housing while the other liquid in the housing flows over the tubes to be heated or cooled. Liquids on the side of the tube and on the side of the bowl are separated by a tube plate.

B. *There are following objective of this research work:*

- The main objective of the study calculated the total heat transfer coefficient.
- Improve the heat transfer rate by using ANSYS CFD.
- During the CFD calculations of the flow in internally ribbed tubes.
- Calculated the temperature distribution and pressure inside the tube by using ansys.

I.RELATED WORK

Neeraj Kumar Nagayach et al. [4] this work provides a summary of the research work of the last decade on the expansion of heat transfer in circular and non-circular tubes. Active and passive methods are wont to increase the heat transfer coefficient within the heat exchanger; Passive methods don't require external power, as within the case of active methods. The effectiveness of the active and passive methods strongly depends on the sort of heat transfer, which may vary from single-phase free convection to the boiling of a dispersed flow film. During this work, the stress is on works involving the staggered use of circular tubes (rotating threaded insert, threaded insert, spiral threaded insert, wire mesh insert), circular (triangular, rectangular) and non-analysis tubes on CFD in laminar and flow.

Nasir Hayat et al. [5] this review of the literature focuses on the applications of CFD within the field of heat exchangers. It's been discovered that CFD is employed within the following investigation areas in several sorts of heat exchangers: misalignment of the liquid flow, pollution, pressure drop and thermal analysis within the design and optimization phase.They need been adopted for the implementation of the simulations. The standard of the solution obtained from these simulations falls within the suitable range, which shows that CFD is an efficient tool for predicting the behavior and performances of a spread of heat exchangers.

Hosseini et al. [6] studied the influence of particle size on deposition in compact heat exchangers. In his work, ANSYS Fluent software was used to solve Navies Stokes equations mediated by Reynolds. Appropriate turbulence models were assessed and a standard epsilon turbulence model with a standard wall function was found appropriate. The semi-implicit equations relating to pressure were chosen as the

coupling scheme for the printing speed. As a result, a numerical investigation has shown that particle deposition increases with increasing particle size.

Ismail et al. [7] in this paper presented are the worked with CFD on compact fins for heat exchangers. Analyzes were performed using Ansys Fluent commercial software to predict the factors f and j for the corrugated and offset fins. Periodic constraints have been applied to eliminate the input effects of the inputs. It is emphasized that there are many correlations between the f and j factors of the band moved in the literature, and these correlations show deviations from each other. Furthermore, new correlations of f ; factors have been developed as a function of Reynolds number and the geometric parameters of the ribs for the wavy fins. Finally, these correlations have been compared with other correlations from the literature.

Rao et al. [8] studied the factors few of the compact fin heat exchanger for single fins using CFDs. In their study, only simple fins were considered. The rectangular flow geometry was modeled taking one quarter of the section due to symmetry. The analyzes were performed using a standard k standard swirl model with better wall function close to the wall treatment. The model was validated with experimental data from the literature, therefore new correlations of the factors f and j were presented for the smooth rectangular fins.

Girgin [9] studied the effects of the configurations of the vortex generators of compact heat exchangers on the heat transfer via CFD. In his office; the common upward flow, the common downward flow and the orientations of the mixed vortex generators with different angles of attack were analyzed. Additionally, the number of vortex generator pairs has been increased from two to three. Ansys Fluent was used as a CFD tool. As a result, three pairs of common drainage configurations with 30° and 45° attack angles gave the best heat transfer performance.

Yaïci et al. [10] investigated the effects of incorrect flow distribution on heat exchanger performance. They examined fin and tube heat exchangers using CFDs. The distributions of the intake air flow and the geometric parameters were mathematically analyzed for various longitudinal, transverse and lamellar slopes. The Coburn factor j , the fan-shaped friction factor and the j / f factor were determined by the analyzes. Flow misalignment and geometric parameters have been reported to have a strong impact on thermal and hydraulic performance.

Ozden et al. [11] studied the effects of design parameters on the hull side on pressure drop and heat transfer by CFD. In his study, numerous CFD simulations were performed to predict the most appropriate turbulence model. The results were compared with the analysis results obtained with the Bell Delaware method. Two impact cutoff values and the relationship between impact distance and hull diameter with different flow rates were examined. The k - f turbulence model feasible with a fine mesh network and spatial discretization of the first order was found to be the best method compared to the results of the Bell-Delaware analysis..

Rehman et al. [12] examined an undisturbed tube bundle heat exchanger with CFD. The heat exchanger contained 19 smooth pipes and a 5.85 m long hull. A network independence study and a series of CFD analyzes were performed and the results were compared with the experimental results. Different turbulence models with different wall treatments were also examined and it was found that the turbulence model of the k -shear stress transport gave better results than the other models. Another conclusion from the CFD analysis was that $2/3$ of the envelope's lateral flow bypassed the tubes and caused an ineffective heat transfer. As a result of this study, changes were made to the design of the heat exchanger to improve heat transfer.

METHODOLOGY

In this study, the design process of a heat exchanger will be theoretically examined, therefore its performance will be analyzed and optimized using computer-assisted fluid dynamics. A countercurrent heat exchanger was considered for design purposes and its length was theoretically calculated using the LMTD method. In this study, the HE30 heat exchange model was initially designed according to a permeable study and the HE30 model was validated. Then change the cutting speed of the deflectors up to 40%. The temperature contours show the outlet and intake temperatures of the heat exchanger with different deflector cutting conditions. Theoretical and CFD results showed only a 1.15% difference in the cooling performance of hot fluids. The axial pressure drops showed positive correlations with the total heat transfer coefficient and the required pumping power. Overall, the results of this study confirm that CFD modeling can be promising for the design and optimization of heat exchangers and that it can test many design options without producing physical prototypes.

A. Experimentation Algorithm

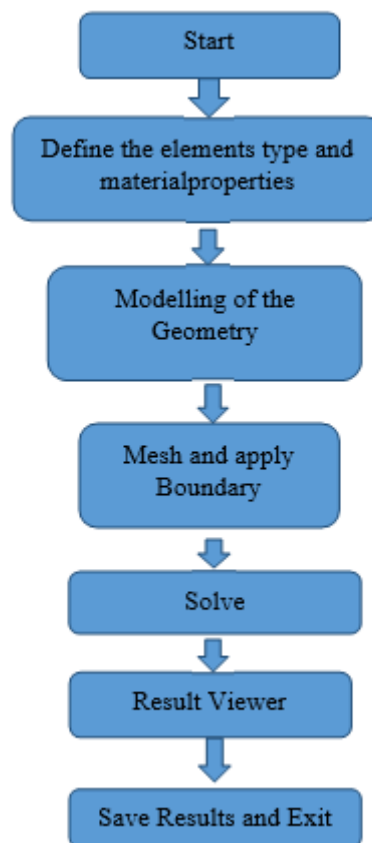


Figure.1. Experimentation algorithm

B. Steps of Ansys Analysis

The different analysis steps involved in ANSYS are mentioned below.

1. Preprocessor

The model setup is basically done in preprocessor. The different steps in pre-processing are

- Build the model
- Define materials
- Generation of element mesh

1. The Model
 - Creating a solid model within Catia

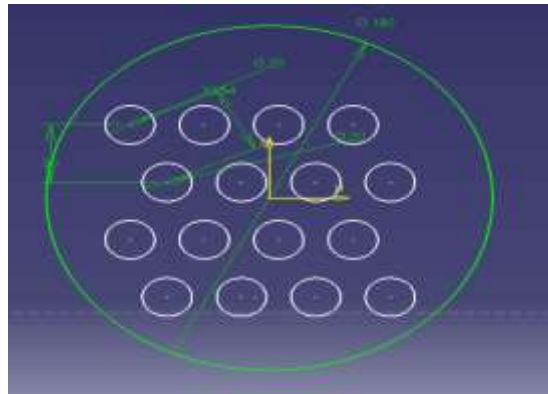


Figure. 2 CAD model prepared in Catia (base paper model)

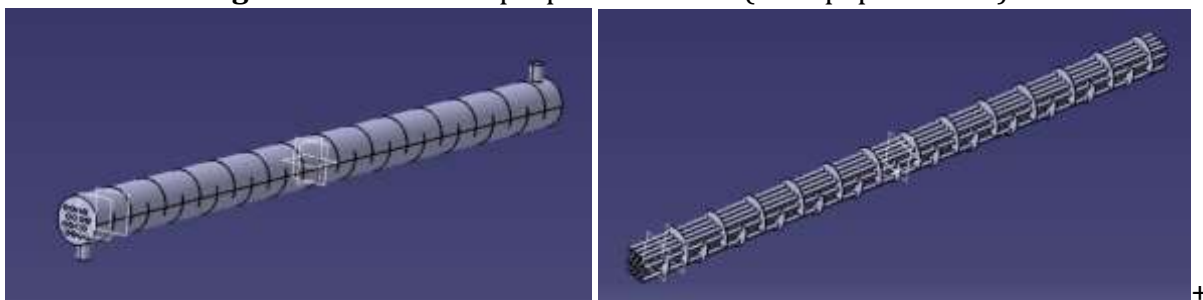


Figure. 3 CAD model prepared in CATIA

2. *Mechanical Properties of fluid*

Table 1. Mechanical Properties of Fluid

Properties	Value
Ph Density (kg/m ³)	1672
PC Density (kg/m ³)	0.275
Thavg	353.15 K
Tcavg	302.8K
CPh	4197 J.kg-1 K-1
CPC	4197 J.kg-1 K-1
uh	0.355X10 ³ Pa.s
uc	0.718X10 ³ Pa.s

3. *Boundary Condition*

1. Define boundary conditions.

In the previous paper, HE30 case was given the best result.so first validated the HE30 case result by using HE30 boundary conditions. Given in the table below. In current study working on different baffle cut ratio. The cut ratio increase the heat transfer rate and also improve the performance of the heat exchanger

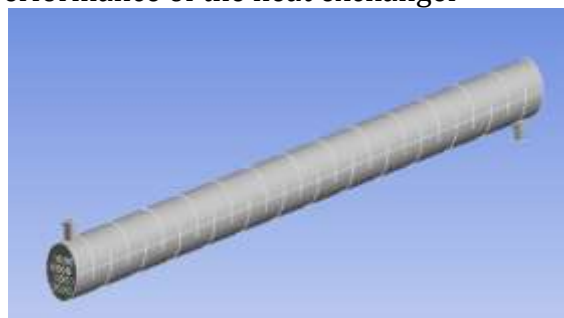


Figure. 4. Cad model import into ANSYS

Apply inlet boundary conditions for CFD analysis

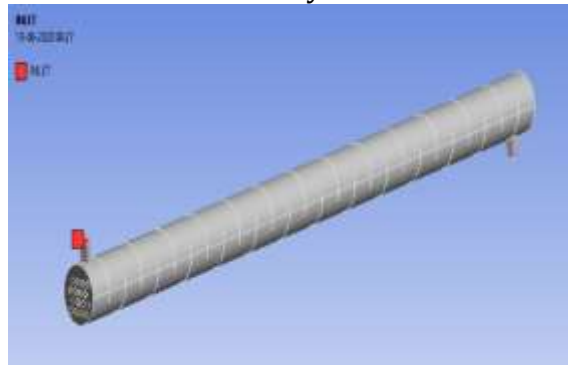


Fig.5. Shell inlet

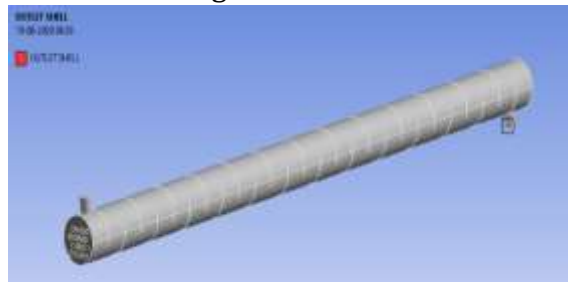


Figure. 6 Shell outlet

Apply inlet boundary conditions for CFD analysis

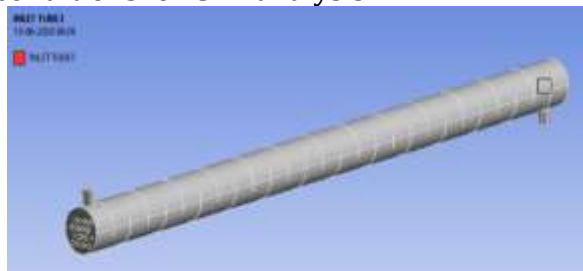


Figure. 7 Tube inlet

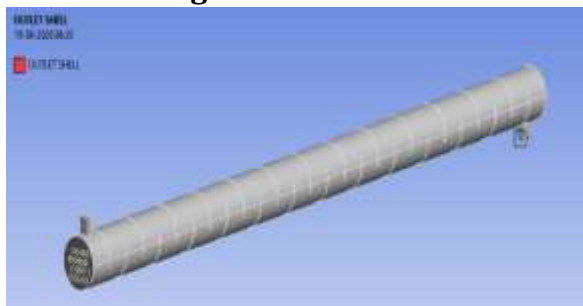


Figure. 8 Tube outlet

HE 30 CAE boundary conditions for base pape.

Table 2 boundary conditions

Boundary conditions	value
V inlet shell	1.25m/s
V inlet tube	0.25m/s
Shell inlet temperature	353k
Tube inlet temperature	302k

4. Validations

Point for paper validations: -

- Build HE30 cad model according base paper.
- In HE 30 case:-
 1. Number of baffles: -25
 2. Baffle cut of rations:-30%
- Validated outlet temperature of the shell and tube. Shown in the table below.

	Shell temperature (K)	Tube temperature (K)	Pressure (Kpa)
base paper	313	332.42	5
Validations Result	309	332	4.5

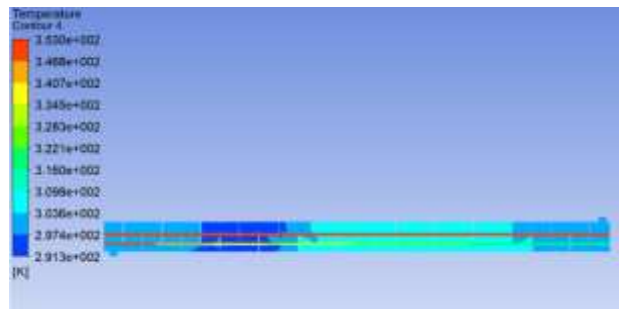


Figure. 9 Temperature contours

Average outlet temperature of tubes:-332.42K

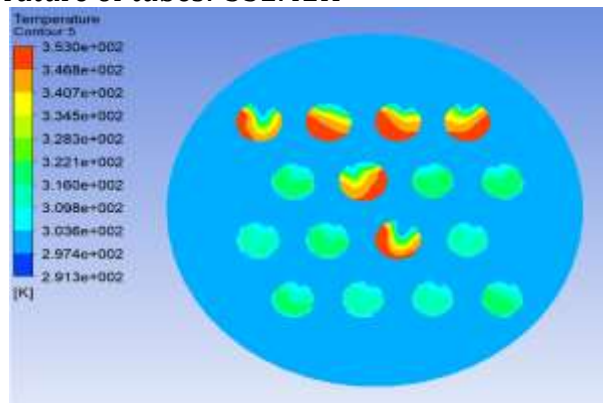


Figure. 9 Tube outlet temperature contours

Average outlet temperature of Shell:-309K

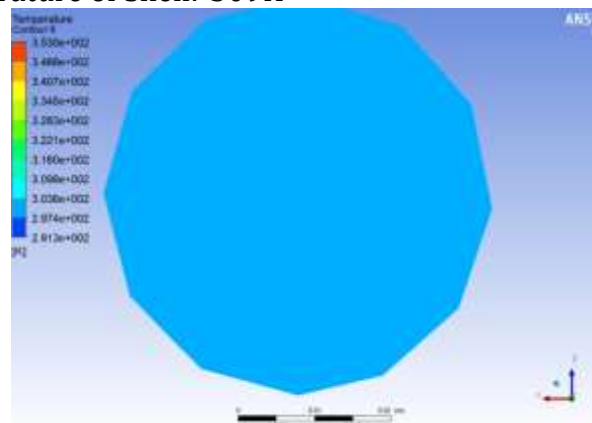


Figure. 10 Shell outlet temperature contours



Figure. 11 Pressure contours

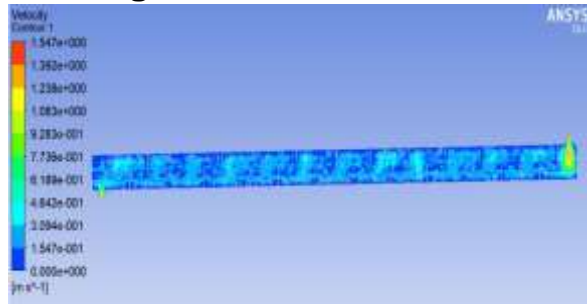


Figure. 12 Velocity contours

5. *Case-1*

In case-1 number of baffles 25 and cut ratio was 20%.and average temperature of the shell outlet temperature was 315k.and tube temperature 327k.

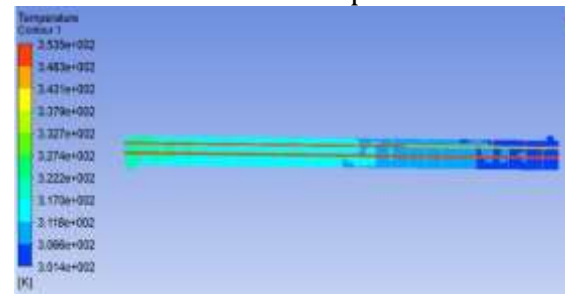


Figure. 13 Temperature contours



Figure. 14 Pressure contours

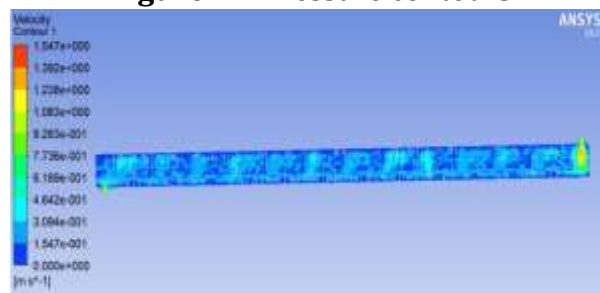


Figure. 15 Velocity contours

6. Case-2

In case-2 number of baffles 25 and cut ratio was 25%.and average temperature of the shell outlet temperature was 305k.and tube temperature 335k



Figure. 16 Temperature contours

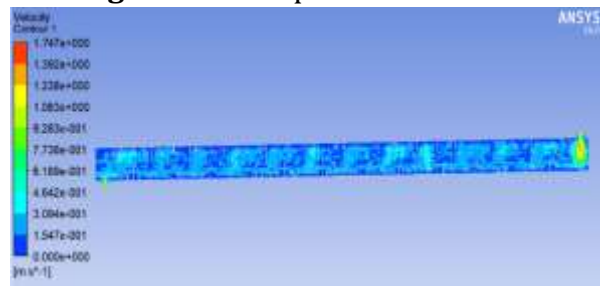


Figure. 17 Velocity contours

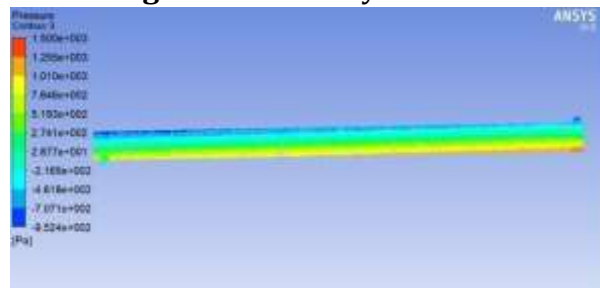


Figure. 18 Pressure contours

7. Case-3

In case-3 number of baffles 25 and cut ratio was 35%.and average temperature of the shell outlet temperature was 298k.and tube temperature 340k.

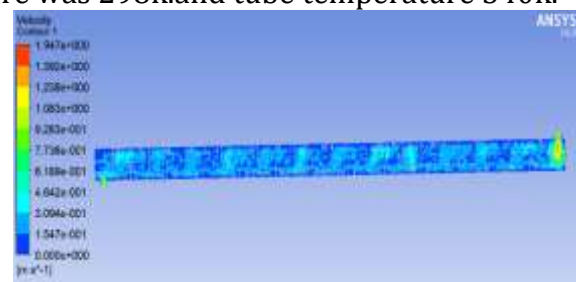


Figure. 19 Velocity contours



Figure. 20 Pressure contours

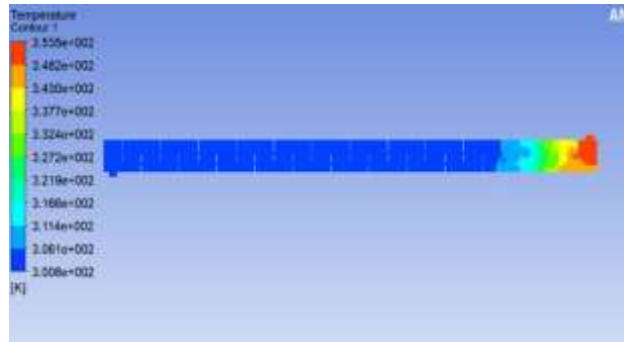


Figure. 21 Temperature contours

8. *Case-4*

In case-4 number of baffles 25 and cut ratio was 40%.and average temperature of the shell outlet temperature was 302k.and tube temperature 337k.

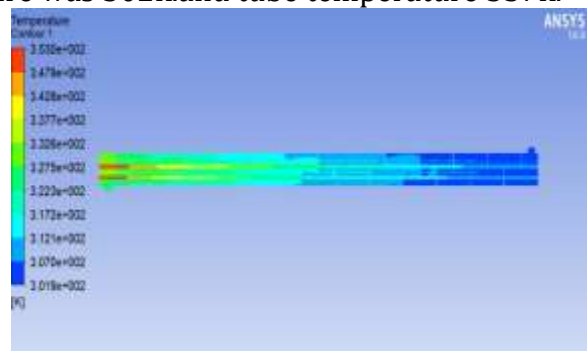


Figure. 22 temperature contours

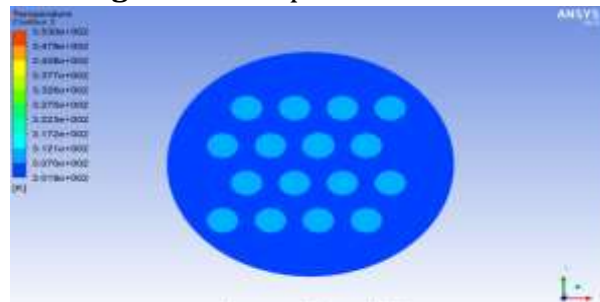


Figure. 23 Outlet temperature of tubes

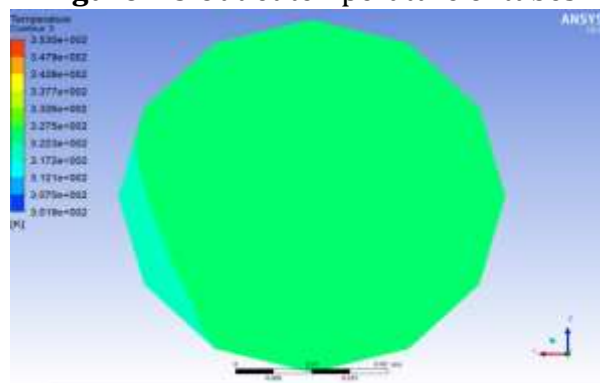


Figure. 24 Outlet temperature of Shell

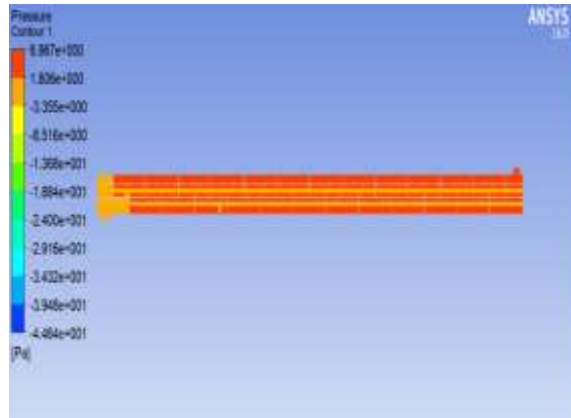


Figure. 25 Pressure contours

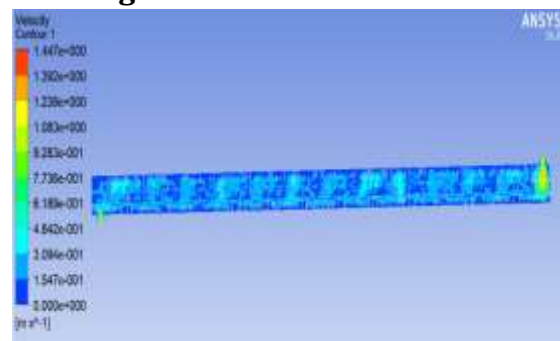
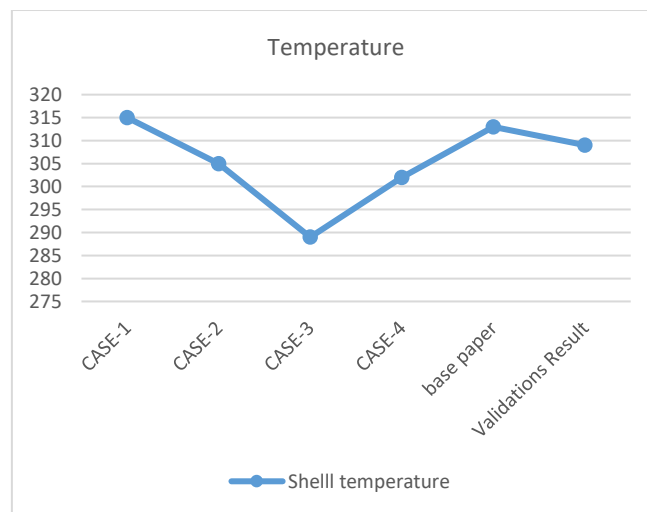


Figure. 26 Velocity Graph

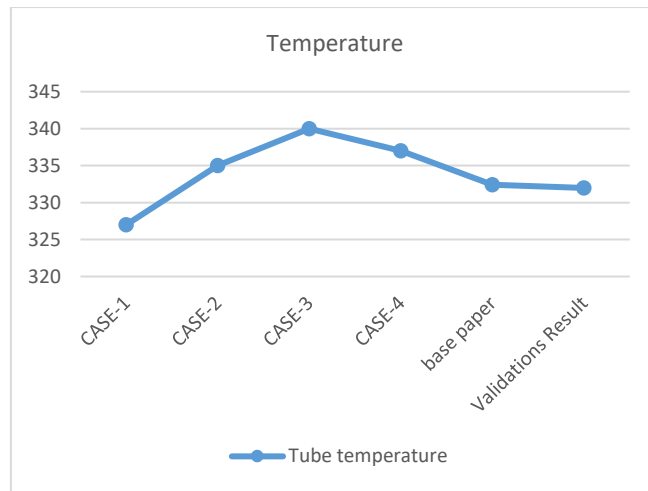
RESULTS

In case 1 to 3 shell temperature decreases and tube temperature increase due to change in heat transfer rate. The graph1 show the shell outlet temperature. And graph 2 show the tube outlet temperature.

	Shell temperature (K)	Tube temperature (K)	Pressure (Kpa)
CASE-1	315	327	2
CASE-2	305	335	2
CASE-3	289	340	3
CASE-4	302	337	3
base paper	313	332.42	5
Validations Result	309	332	4.5

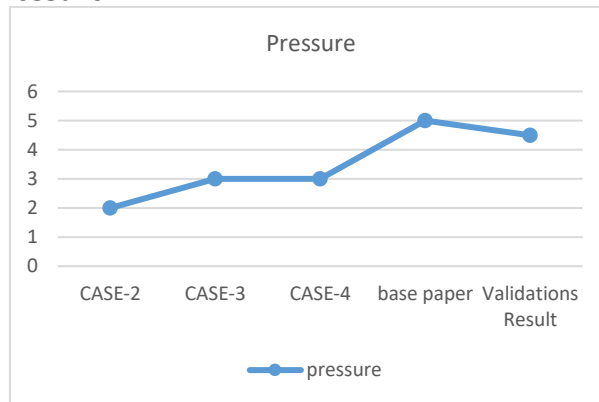


Graph. 1 Shell temperature graph

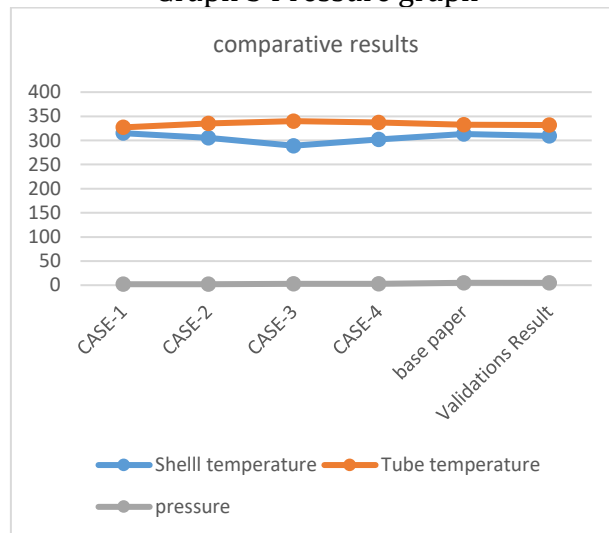


Graph 2 Tube temperature graph

In case 1 to 3 shell pressure increase due to change in heat transfer rate. The graph 3 show the shell axial pressure.



Graph 3 Pressure graph

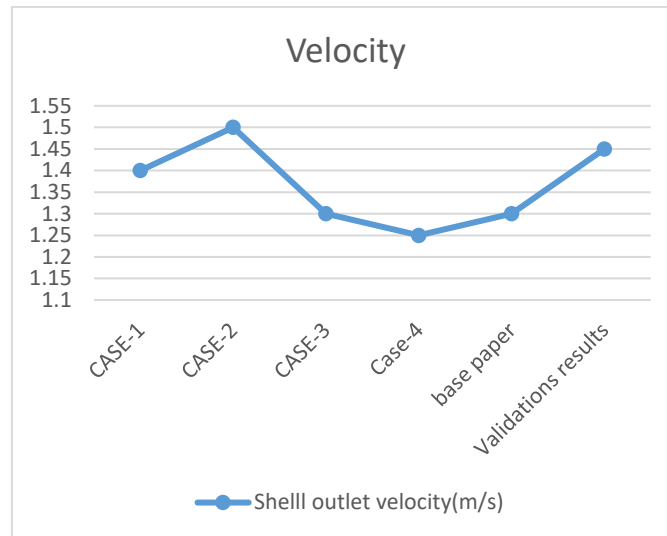


Graph 4 Comparative result graph

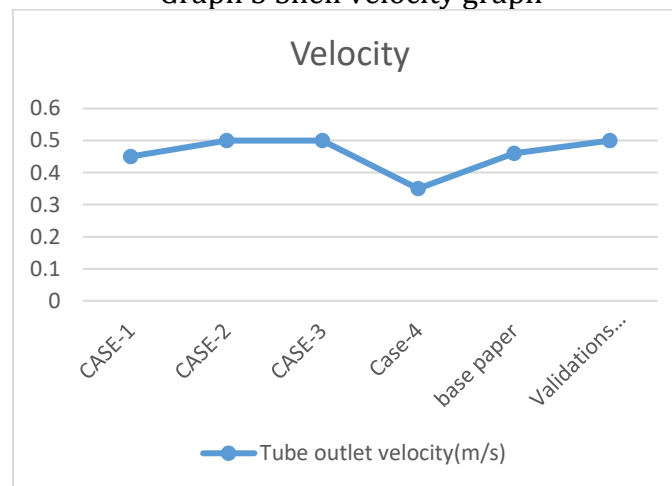
In case 1 to 3 shell velocity decreases due to change in number of baffles. The graph 5 show the shell outlet velocity. And graph 6 show tube outlet velocity.

	Shell outlet velocity(m/s)	Tube outlet velocity(m/s)
CASE-1	1.4	0.45
CASE-2	1.5	0.5

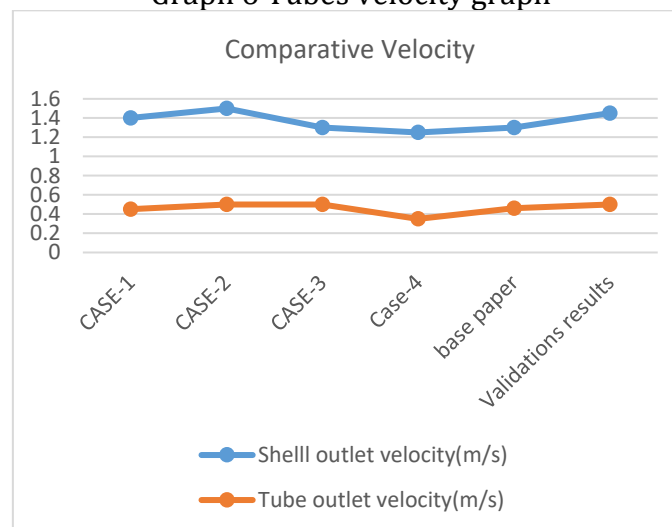
CASE-3	1.3	0.5
Case-4	1.25	0.35
base paper	1.3	0.46
Validations results	1.45	0.5



Graph 5 Shell velocity graph



Graph 6 Tubes velocity graph



Graph 7 Comparative results

CONCLUSION

Basic knowledge in thermodynamics, fluid dynamics, and CFD are obviously crucial for the design and optimization of a compact heat exchanger. In this work, three CFD models were developed and their accuracy was validated by a detailed theoretical calculation. Based on the results of the CFD, it has been recognized that careful selection of parameters such as the deflector cut ratio, the number of deflectors and pipes, the flow rate and the layout of the pipes is crucial to optimize performance. A tube bundle heat exchanger for a certain period of time. Of the three CFD models tested, the CASE-3 CFD model (with a diaphragm cutting speed of 35%, 16 tubes and 25 deflectors) gave the best results in completing the desired task, which is in good agreement with the theoretical results. A reduction in the cutoff frequency by impact increases the heat transfer coefficient on the side of the casing, but this also leads to an increase in the pressure drop. Obviously, the number of tubes used in a heat exchanger has an impact on the flow of the tube to maintain the required mass flow. The lower the number of pipes, the greater the pressure drop for a specific activity. It is even more important that the results of this work agree with the research results previously reported and this demonstrates the accuracy of the results obtained. Overall, the results of this work confirm that CFD modeling is promising for the design and optimization of a heat exchanger.

FUTURE SCOPE

The total heat transfer rate of the heat exchanger is depend on the baffle design. For future study the design of the baffle also optimized by using ANSYS fluent. The changing in angle of baffle will also improve the total heat transfer rate and optimized the overall heat transfer rate.

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